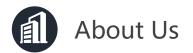


Herch Opto Electronic Technology Co., Ltd

World's Leading Fiber Optic Temperature Sensing & Measurement Solution Provider







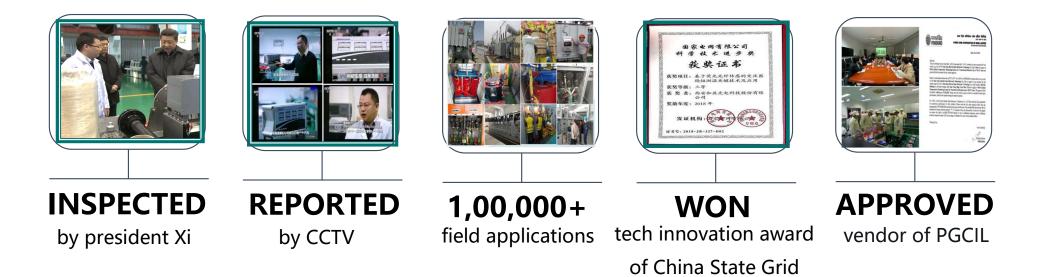
Incubated by Chinese Academy Of Science in 2011



Biggest fiber optic temperature sensing solution provider in China



Hold over 100 patents, has its own known-how







Factory Building



FO Sensor Production Line

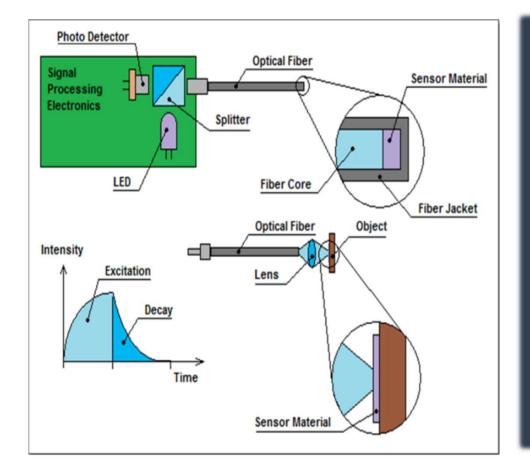


Temperature Monitor Production Line



Testing & Calibration





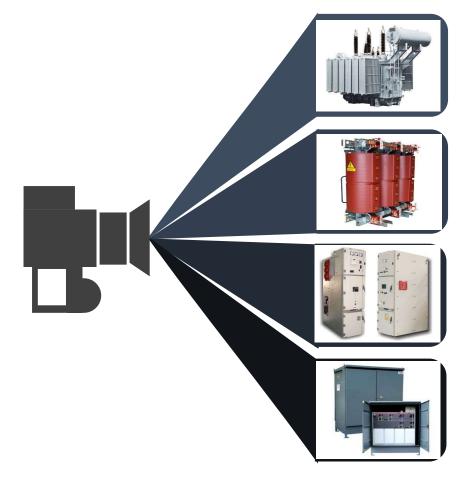
PRINCIPLE

Our fiber optic temperature sensors are based fluorescence decay technology.

Upon being stimulated by a light source, electrons inside the sensitive rare earth material absorbs photons, which move from a low to a high state of energy. When they return to the low state, they fluoresce. When the stimulation stops, the fluorescence begins to attenuate exponentially.

The duration of attenuation is temperature dependent only. And the temperature can be found out by monitoring the duration of the fluorescence.





Oil immersed transformer temp. measurement

Cast resin transformer temp. measurement

Switchgear temperature measurement

RMU temperature measurement





Standard Test Procedure for Thermal Evaluation of Oil Filled Transformers

$$LIFE = EXP^{\left[\frac{15\ 000}{T+273} - 27.064\right]}$$

where

LIFE is the life in hours T is the hottest-spot temperature in °C

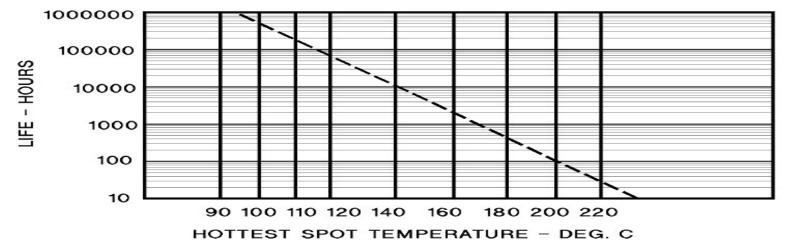
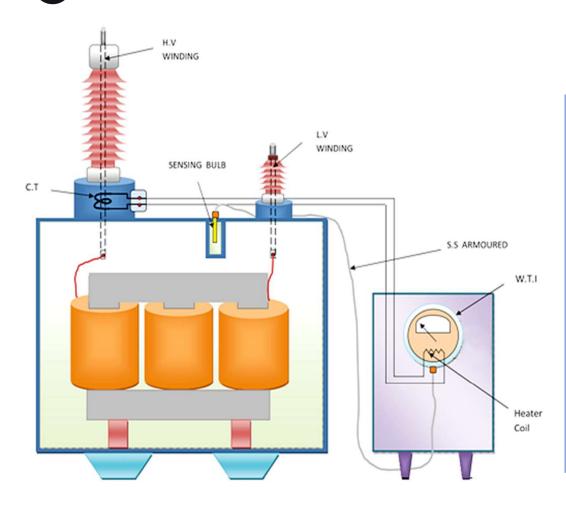


Figure 1—Minimum life expectancy curve for liquid-immersed distribution, power, and regulating transformers rated in accordance with IEEE Std C57.12.00-1993, 65 °C average rise, 80 °C hottest-spot rise



Conventional Method-WTI





01 Use CT from one phase and top oil to simulate hot spot
02 Based on simulated values
03 Top oil has significant time lag related to winding real temperature (indicate temperature measurement)
04 Inaccurate range from 5 to 20°C





IEC 60076-2 Recommendations on fiber optic sensors installations

Table E.1 – Minimum recommended number of sensors for three-phase transformers

Rated power MVA	Cooling system	Number and phases of installation				
		Total	On central phase		On each lateral phase	
			HV winding	LV winding	HV winding	LV winding
≥ 100	All system	8	2	2	1	1
From ≥ 20	ON – OF	6	1	1	1	1
to < 100	0D	8	2	2	1	1







Temperature Range	-40°C-260°C		
Temperature Accuracy	±1℃		
Temperature Resolution	0.1℃		
Number of Channels	Up to 16 channels		
Temperature Unit	°C or °F		
Display Mode	Digital tube display, display directly if less than 8 channels, display in turn if more than 8 channels		
Response Frequency	2 seconds per channel (Depend on probes' position)		
Power Supply	24V DC (with AC/DC convertor)		
Interface	RS-485 Ethernet 4-20mA (each channel) Optical connector 8 programmable relays		
Memory	1GB memory space, USB port accessible		
Power Consumption	≤10W		
Communication Protocol	Modbus, IEC 61850		
Fiber Optic Length	1 to 25m		



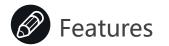
01 Does not or will not carry electrical current

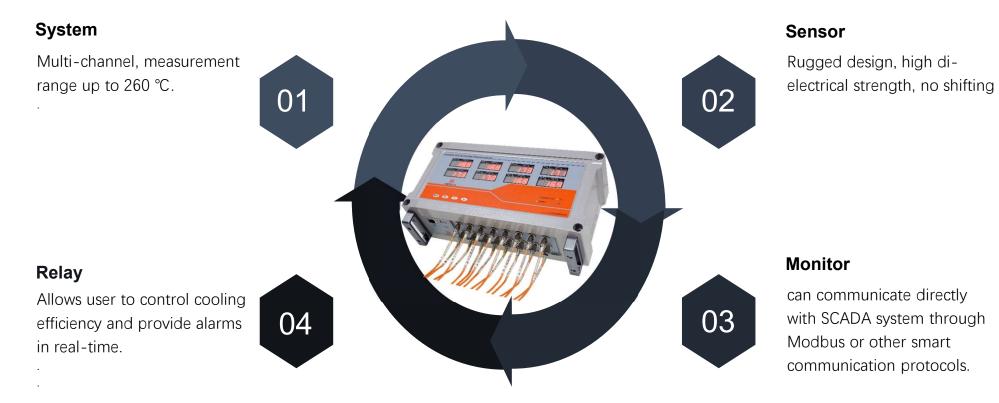
- 02 Immune to EMI, microwave, radio frequency, vibration, radiation
- O3 Can be positioned in hard-to-reach or view places



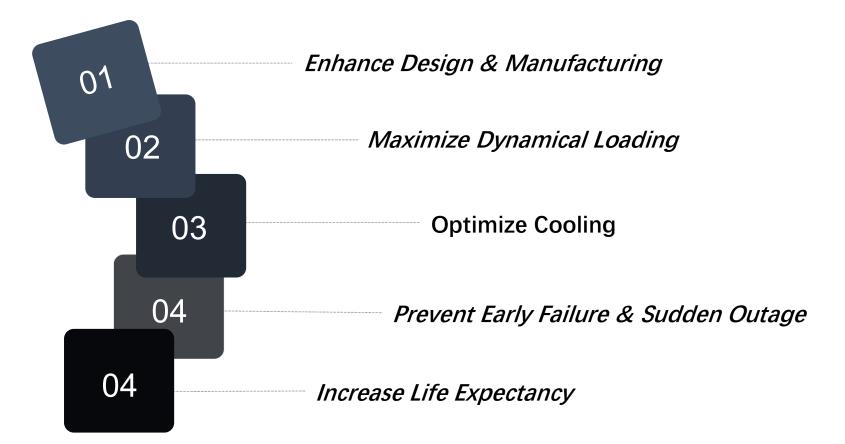
Can measure small or precise locations













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Negative Lightning Impulse:

Ten (10) samples were dried and impregnated per ASTM D2413 and tested per ASTM D3426, <u>Test</u> <u>Method for Dielectric Breakdown Voltage & Dielectric Strength of Solid Electrical insulation Maternals</u> <u>sugn impute Wave</u>. Samples were passed through the center of two 51 mm diameter electrodes with a 25 mm gap (Figure 4). For each sample the tip was tested followed by the cable. A standard 1.2 x 60 us imputes was applied using a HipOrtincis 11 stage Marx openator delivering a maximum of 2500 joules discharge energy. A series of 3 imputes at 400 kV were applied followed by a 20 kV increase and an additional series of 3 imputes. This sequence was continued until 3 successful imputes at 500 kV were achieved. After the cable was qualified at 500 kV, the test was stopped.

Negative Switching Surge:

Ten (10) samples were dried and impregnated per ASTM D2413 and tested per ASTM D3426, <u>Test</u> <u>Method for Dielectric Breakdown Voltage & Dielectric Strendth of Solid Electrical Insulating Materials</u> <u>using Inguitse Waves</u>. Samples were passed through the center of two 51 mm diameter electrodes with a 25 mm gap (Figure 4). For each sample the tip was tested followed by the cable. A standard 250 x 2500 µs impulse was applied using a Hipotonics 11 stage Marx generator delivering a maximum of 2500 jouled sickstange energy. A series of 3 impulses at 300 kV were applied followed by a 20 kV increase and an additional series of 3 impulses. This sequence was continued until 3 successful impulses at 360 kV were achieved. After the cable was qualified at 360 kV, the test was stopped.



Figure 3: AC w/PD test set (left), Negative lightning impulse and switching surge test set (right)

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Figure 1: Tip of fiber optic cables in T4 mask

After testing the tip of each sample, the cable was strung across the center of the 15 mm gap between the Rogowski electrodes using machined polyethylene blocks to hold them in place (Figure 2, right). The same voltage application and PD measurement techniques that were used for testing the tips were used for the cables.

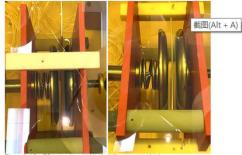


Figure 2: AC w/PD test tank assembly; tip (left), cable only (right)

Summary:

There were no breakdowns observed during AC with partial discharge, negative lightning impulse, or switching surge testing. During AC with PD testing there was no observed partial discharge above the acceptable threshold. Therefore all fiber optic probes tested met the qualification voltages for their respective tests:

- AC with PD; 70 kV (4.7 kV/mm)
- Negative lightning impulse; 500 kV (20 kV/mm)
- Negative switching surge; 360 kV (14.4 kV/mm)



Installation Process

Prepare spacer and fix sensor into spacer



Seal tarfo with tank wall plate, connect inter & exter fiber optic via feedthrough

Connect exter fiber optic cable to temperature monitor



Insert spacer into windings







THANK YOU

